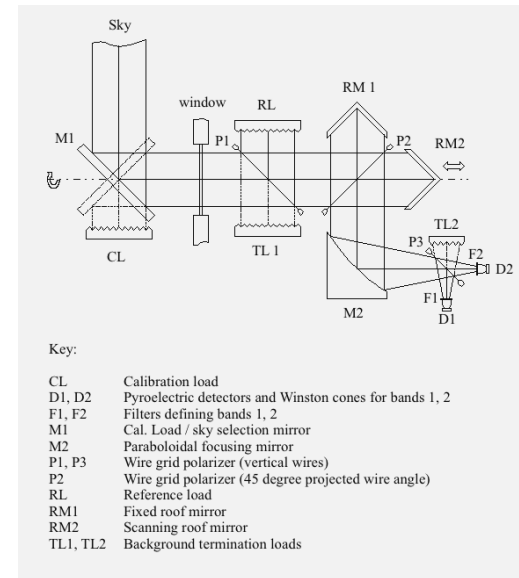


# Atmospheric Modeling and Instrument Design for the Dome A FTS



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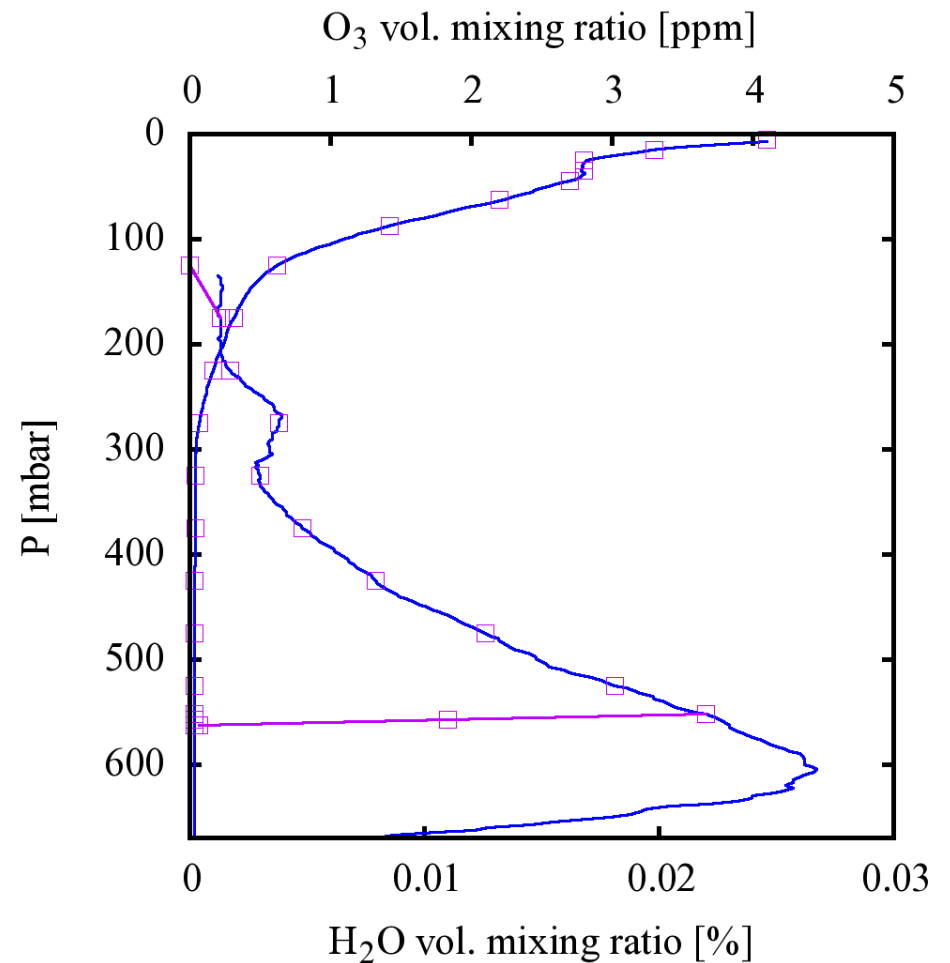
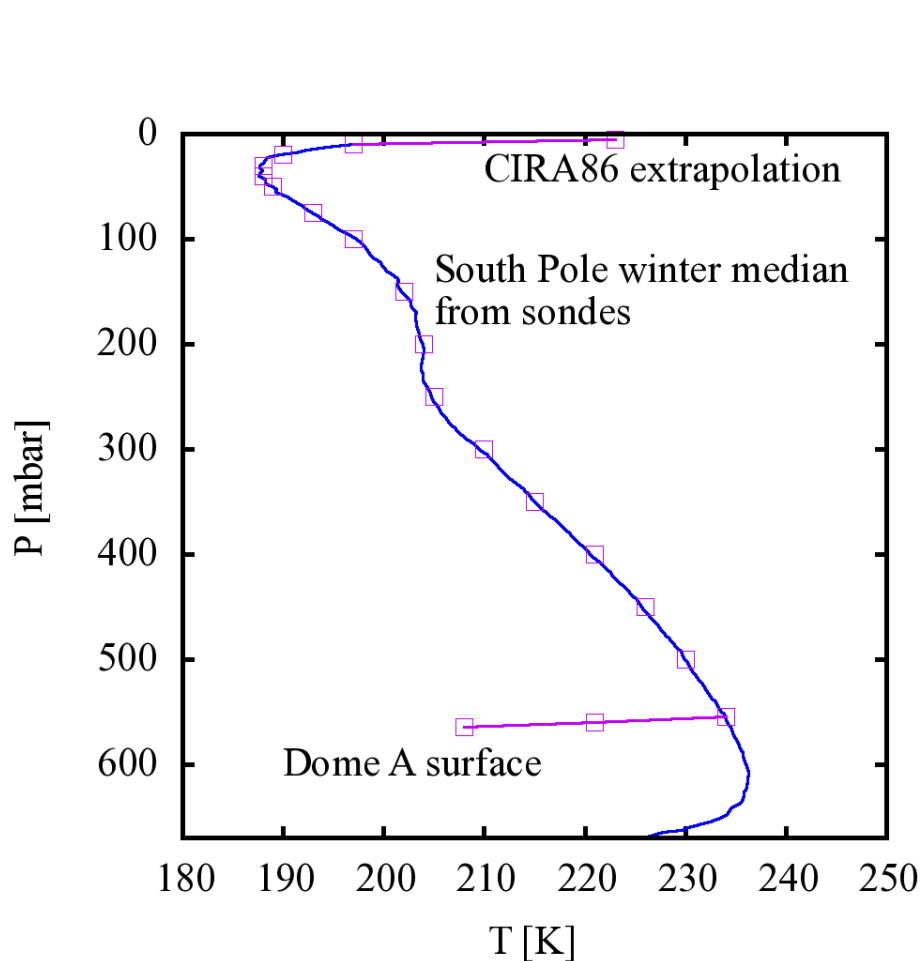
# Outline

- An atmospheric model for Dome A
  - Estimated vertical profiles
  - Absorption by water vapor and other gases
  - Model radiance and transmittance
- FTS Design
  - Design constraints for Dome A
  - Optical layout
  - Sensitivity analysis
- Next steps

# An atmospheric model for Dome A

- Serves as a starting point for instrument design
- Model profiles
  - Start with median winter profiles from NOAA CMDL South Pole ozonesondes, which carry chilled-mirror hygrometers.
  - Ground point based on Dome A weather station data
- Clear sky radiative transfer
  - Show contributions of different components
  - Most uncertain is H<sub>2</sub>O continuum
- Compute using *am* code

# Dome A model profiles (winter median)



- Model surface inversion is 10 mbar thick (e.g. J. S. Lawrence, *PASP* **116** 482 2004)
- Symbols indicate points used for *am* winter median model profiles.
- Model winter pwv quartiles are 115  $\mu$  m, 180  $\mu$  m, 270  $\mu$  m
- Dome A should be drier, and early Pre-HEAT data do imply lower median pwv, so use 75  $\mu$  m in examples

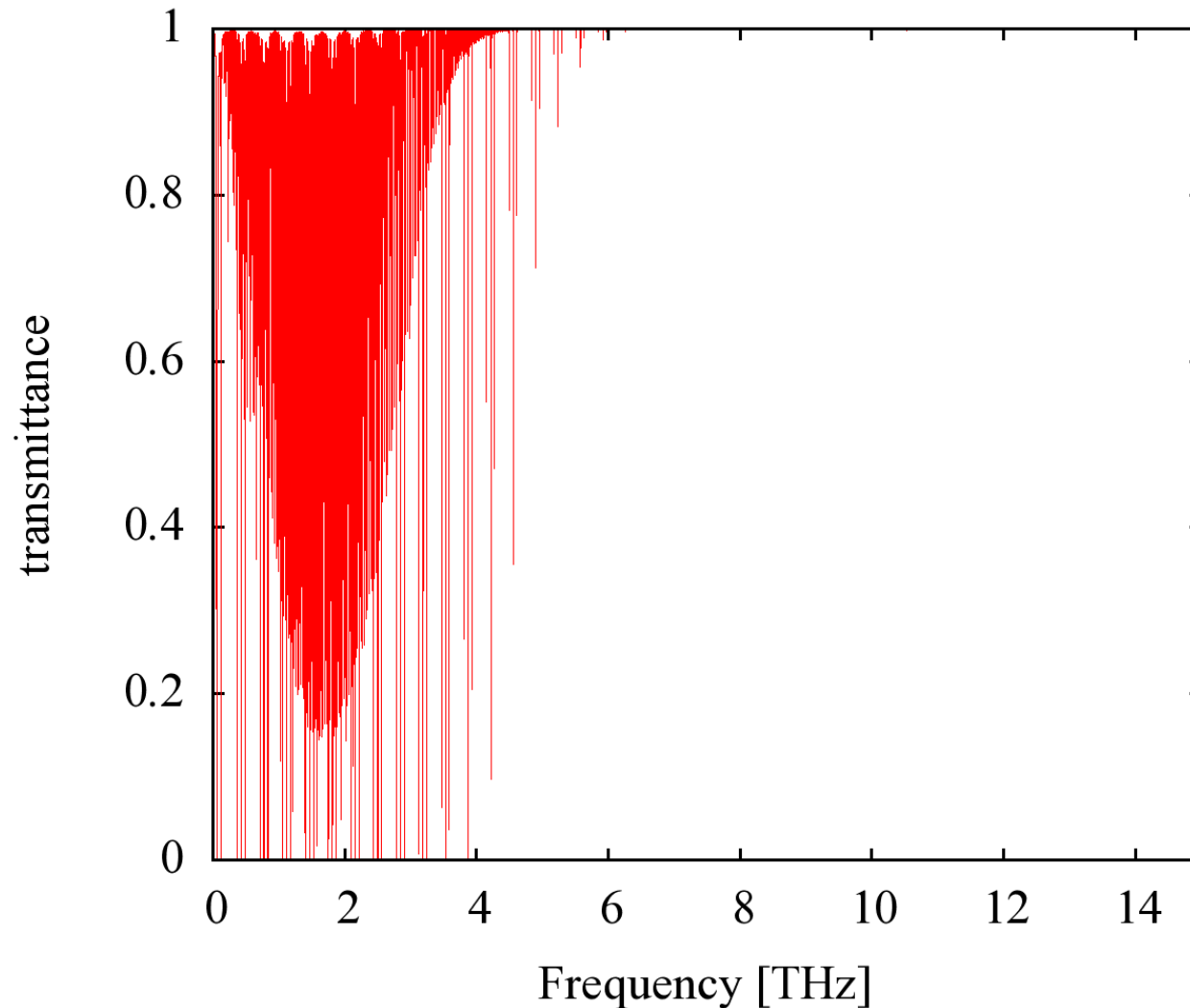
# Atmospheric model absorption

Use model profiles in a radiative transfer model with:

- Dry line-by-line absorption –  $O_2$ ,  $O_3$ ,  $N_2O$ ,  $CO$ ,  $CH_4$
- Dry collision-induced absorption –  $N_2$ ,  $O_2$
- $H_2O$  line-by-line and continuum absorption

Look at each of these in turn, then put it all together...

# Dome A dry line-by-line transmittance



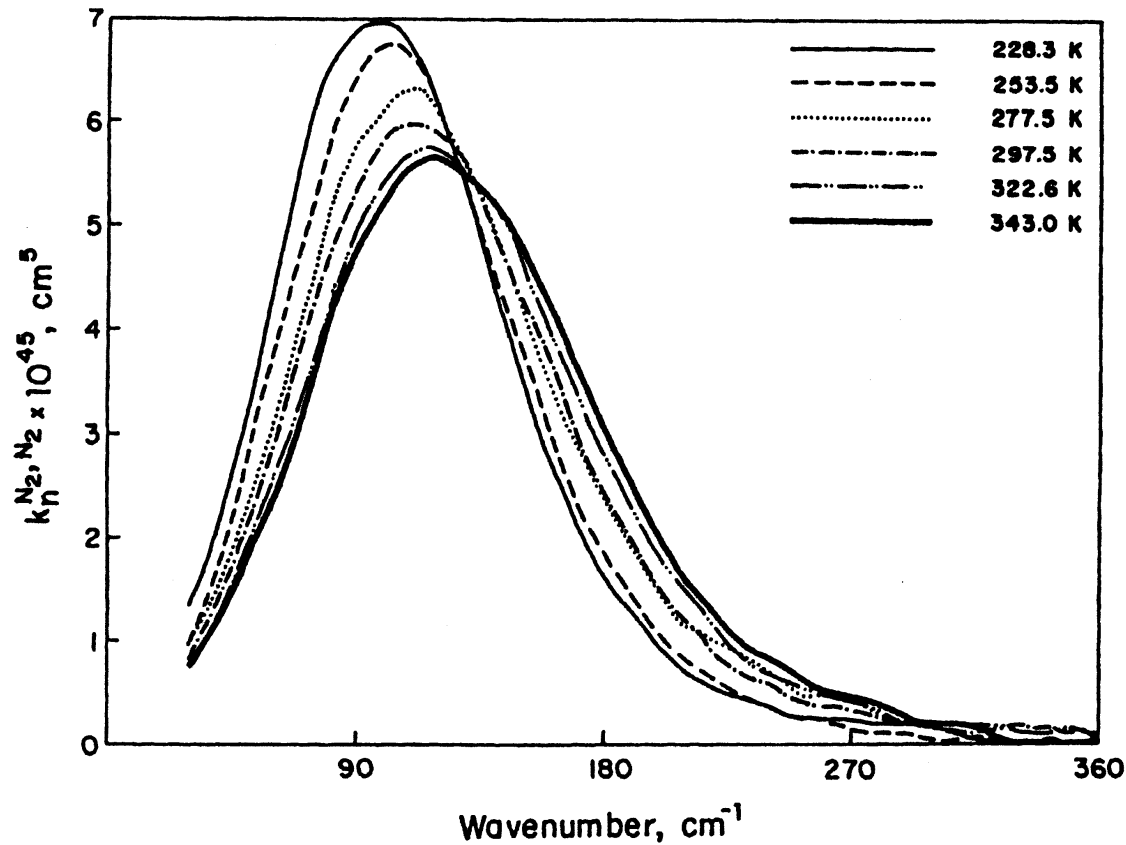
Mainly  $O_2$ ,  $O_3$  pure rotation bands – occupied bandwidth is small

# Collision-induced absorption (CIA)

- Broadband dry THz absorption is mainly  $\text{N}_2\text{-N}_2$ ,  $\text{N}_2\text{-O}_2$  CIA.
- Forbidden electric quadrupole and 16-pole rotational transitions acquire dipole coupling via polarization of collision partner.
- Binary process, so absorption depends on density squared.
- Collisions are brief ( $\sim 10^{-12}$  s), so broad lines blend into an unresolved band.
- $\text{N}_2\text{-N}_2$  lab data is available to 90 K.  $\text{N}_2\text{-O}_2$  can be estimated by scaling.
- $\text{O}_2\text{-x}$  is less well-studied, but its contribution to atmospheric opacity is small.

# Laboratory N<sub>2</sub>-N<sub>2</sub> CIA spectrum

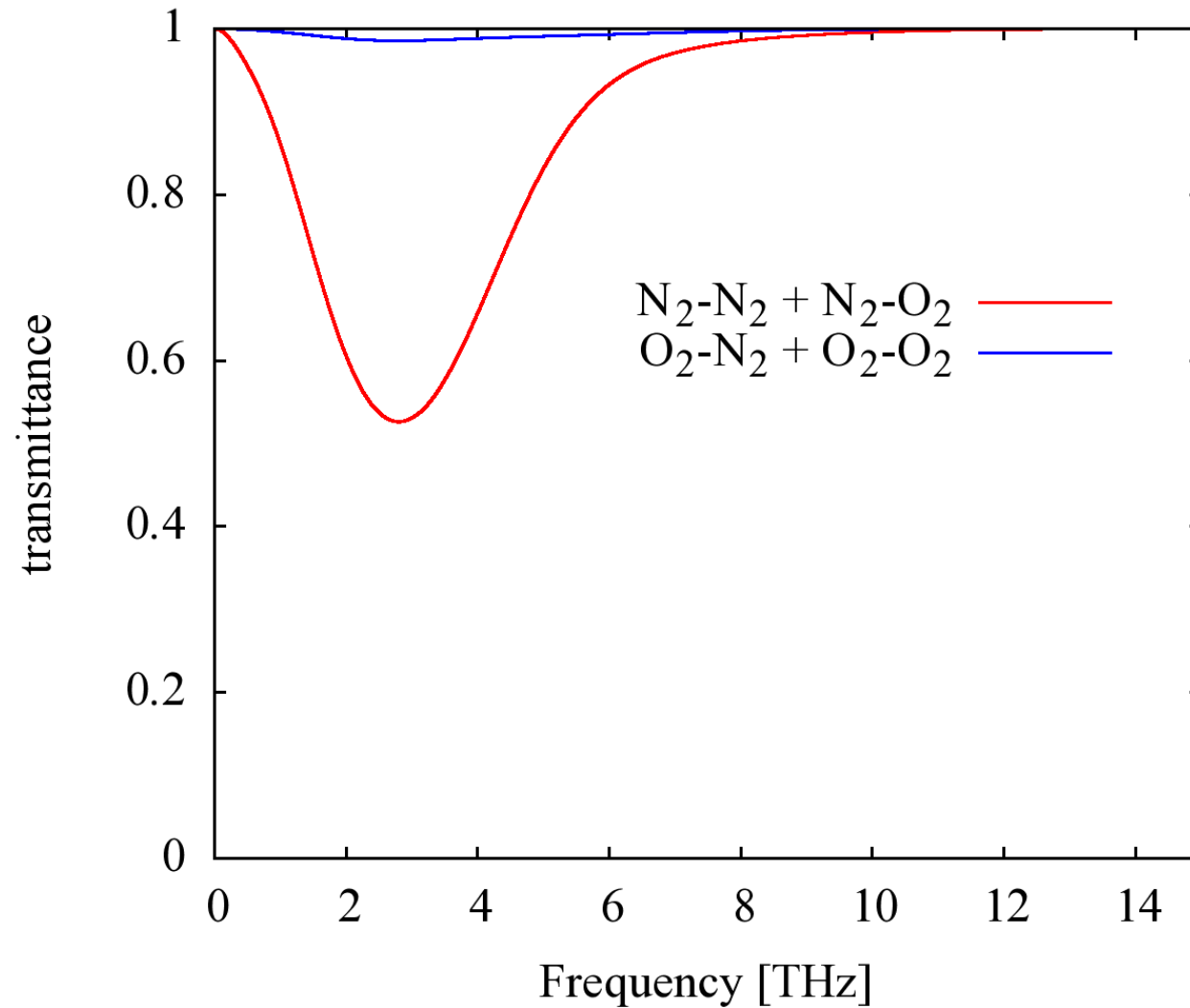
(Stone, et al. 1984)



**FIG. 5.2.** The collision-induced rotation band of pure nitrogen (nitrogen–nitrogen collisions). The vertical axis is the binary absorption coefficient, as defined in (3.88). After Stone et al. (1984).



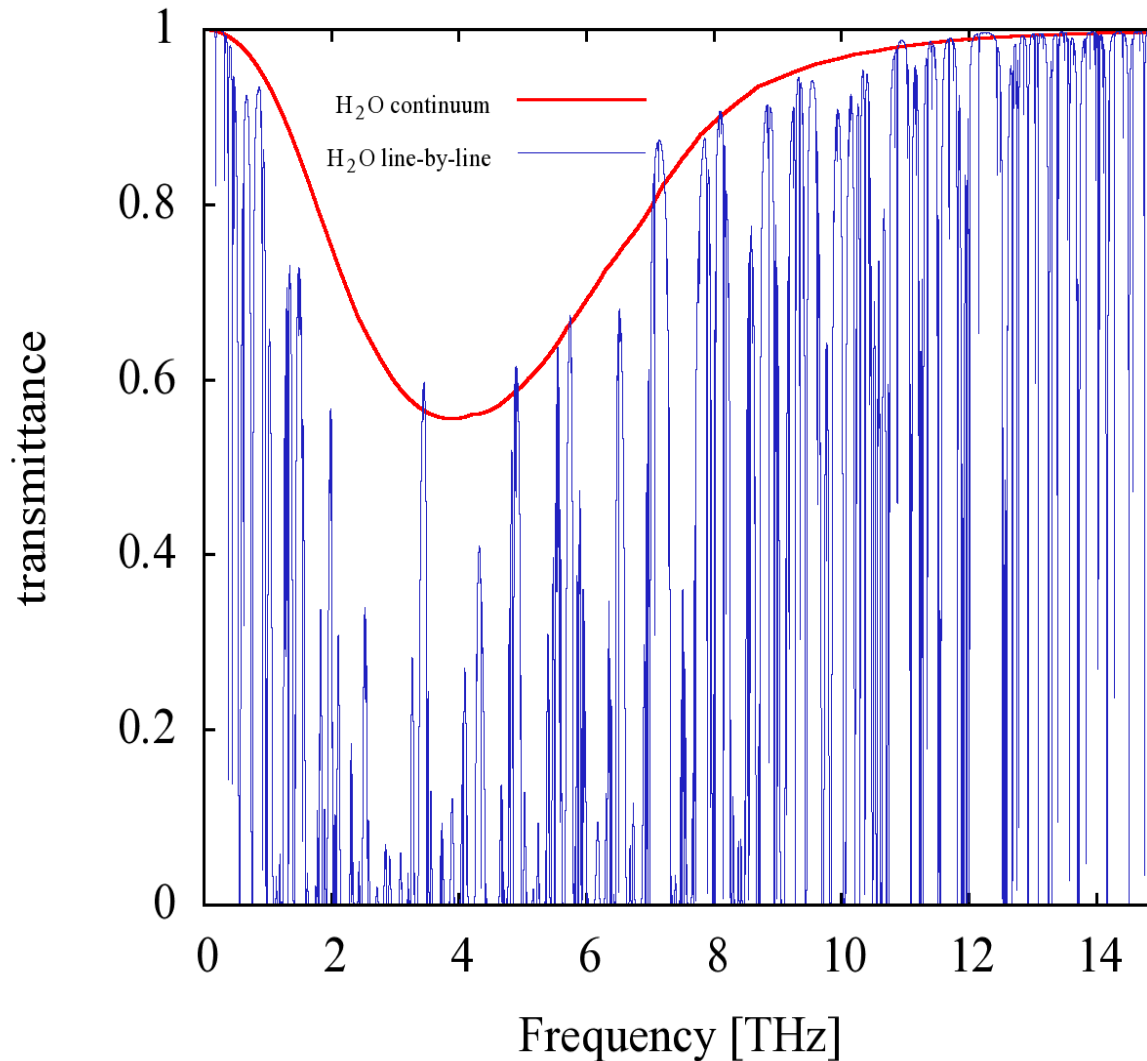
# Dome A winter CIA transmittance



# H<sub>2</sub>O Continuum

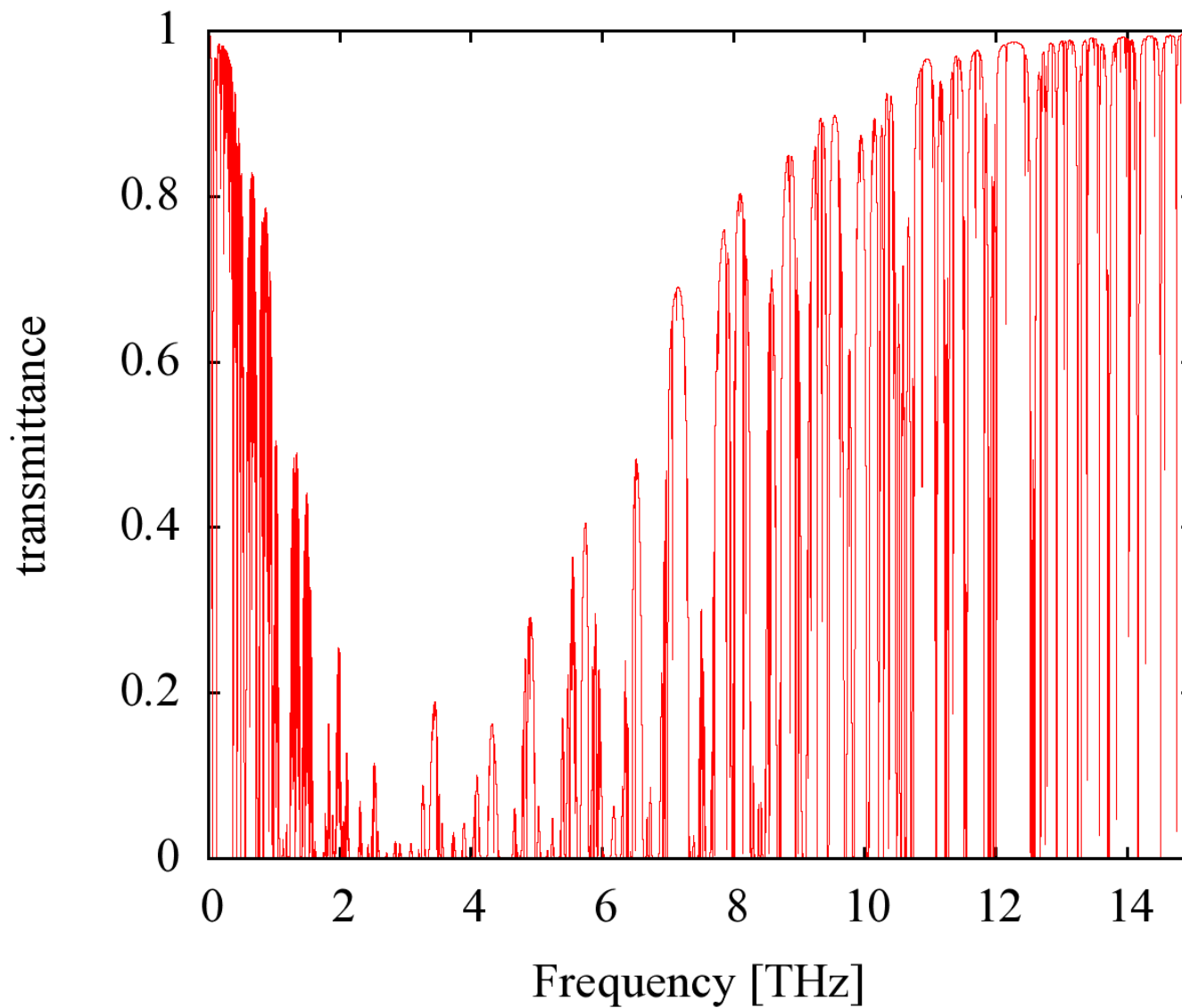
- Associated with short-range collisions
- Dipole-allowed transitions are affected, may also have a CIA component
- Difficult to study experimentally
  - Hard to disentangle from allowed line spectrum
  - H<sub>2</sub>O vapor hard to control experimentally at low T
- Best model is MT\_CKD (Mlawer, et al., see [rtweb.aer.com](http://rtweb.aer.com))
  - Self-continuum defined for  $260 \text{ K} < T < 298 \text{ K}$
  - T-dependence not developed for air-induced continuum, which dominates in the dry conditions at Dome A
  - Probably not accurate at low Dome A temperatures
  - Improvements needed for RT component of climate models

# Dome A H<sub>2</sub>O transmittance (75 μm pwv)

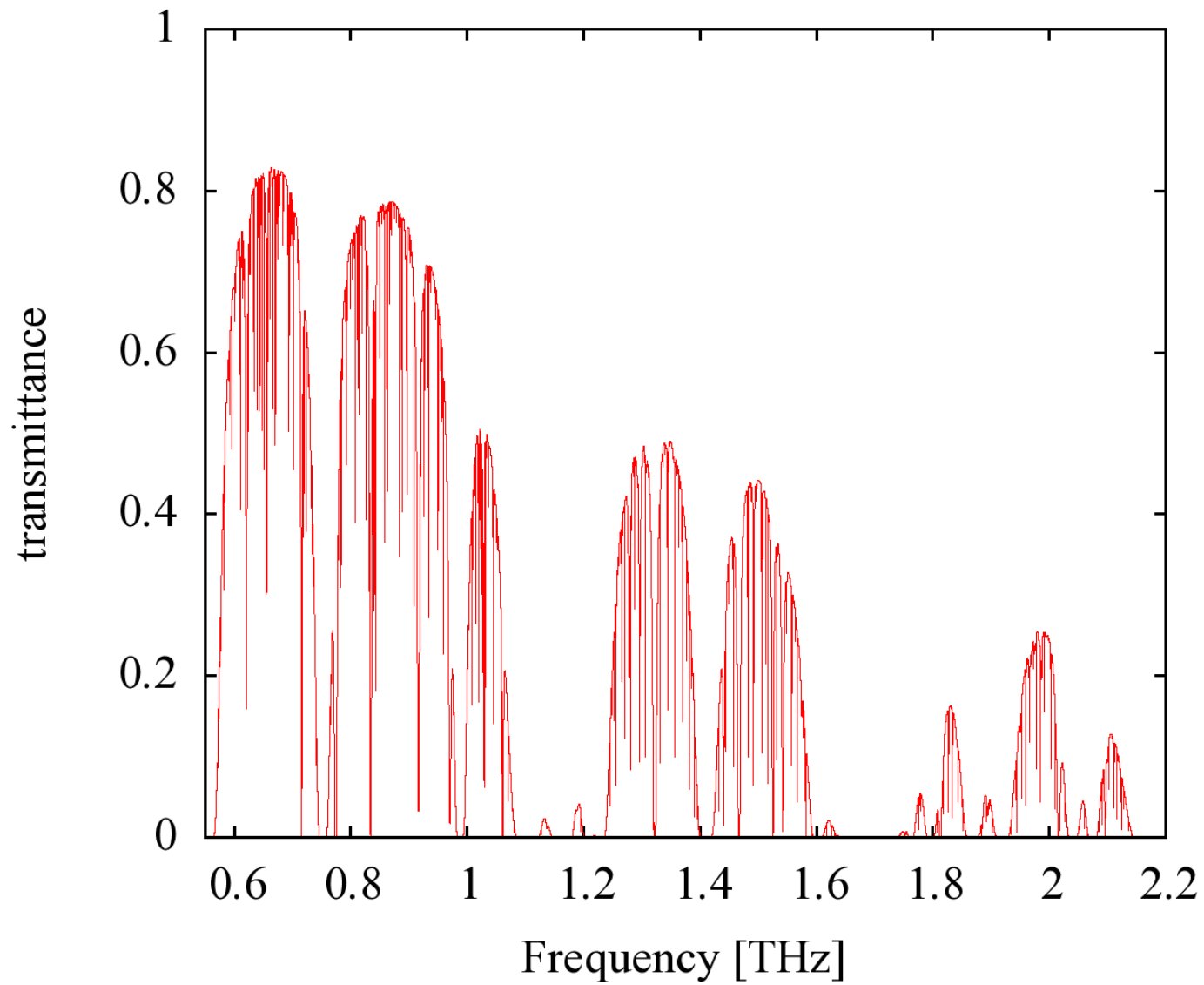


Accuracy of the T-independent MT\_CKD self-continuum is questionable at such low temperatures ( $T < 240$  K). The band can be expected to move down in frequency and sharpen. (Compare with line-by-line.)

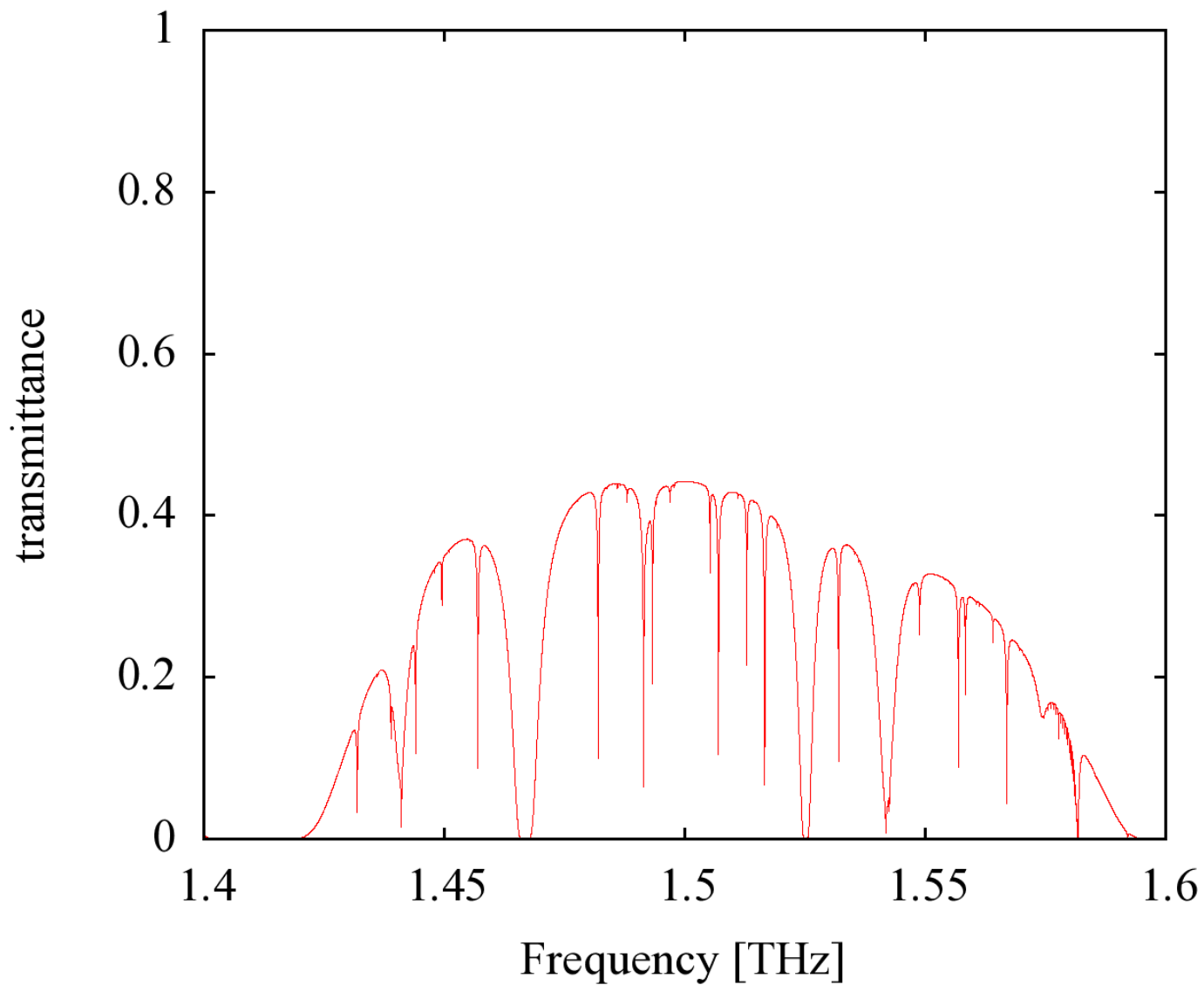
# Net model transmittance ( $75 \mu\text{m}$ pwv)



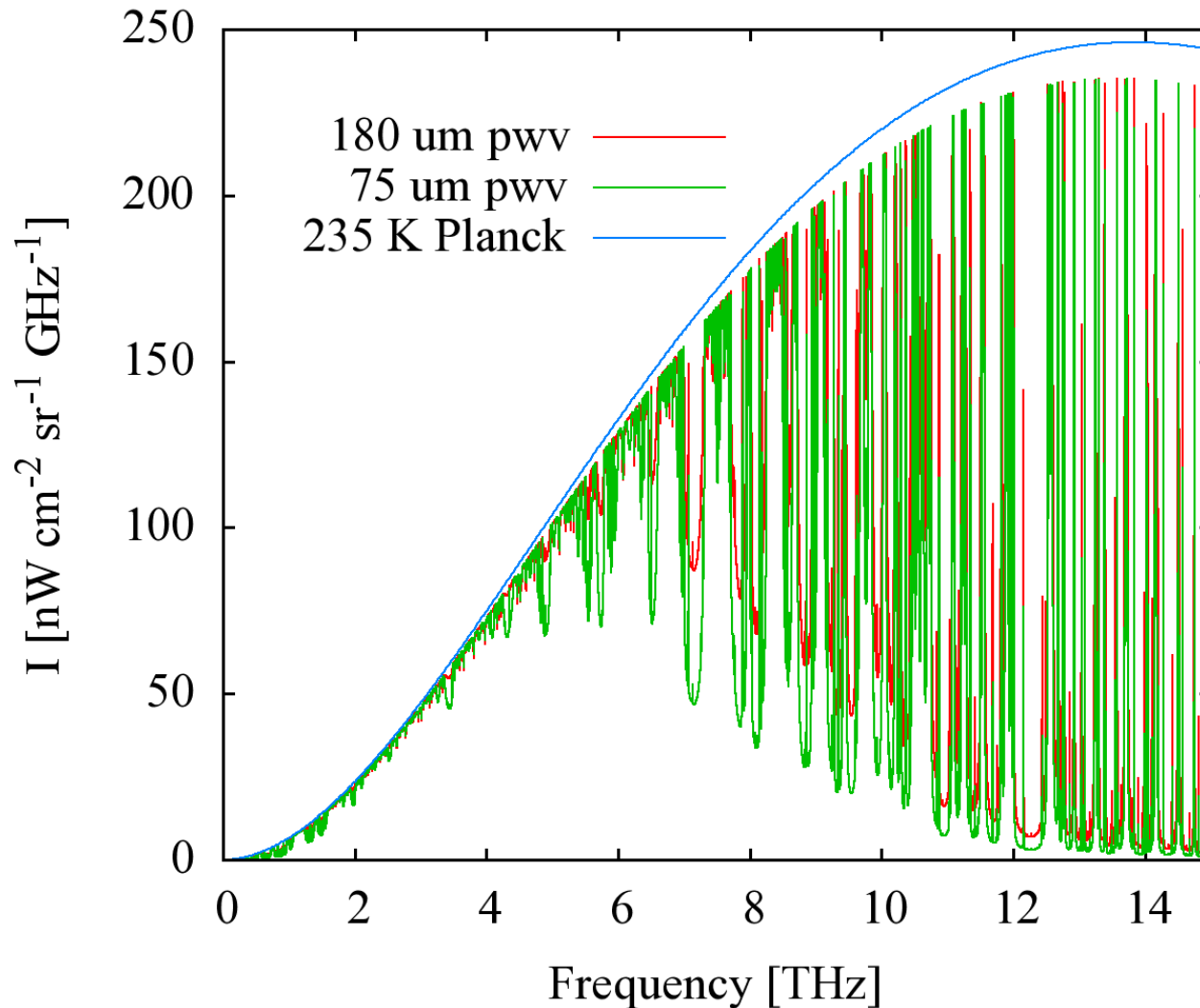
# Net model transmittance ( $75 \mu\text{m}$ pwv)



# Net model transmittance ( $75 \mu\text{m}$ pwv)



# Net model radiance



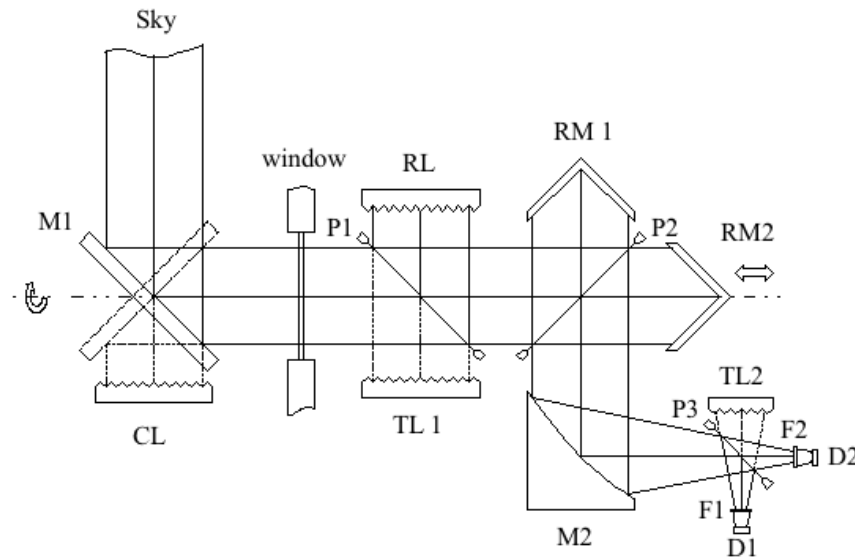
- The large dynamic range in this spectrum is a key design driver for the FTS
- Solution – split into bands

# FTS design considerations

- Dome A requires low power, and no cryogenics
  - ambient temperature pyroelectric detector
  - passive calibration loads
- Broad spectral coverage (0.75 THz – 10 THz)
  - cover both sides of H<sub>2</sub>O rotation band
  - split into bands to reduce dynamic range and maximize low frequency throughput
- Measurement time  $\approx$  10 minutes / spectrum
  - drives optical throughput, spectral resolution, and low-frequency cutoff



# Optical design concept



CL	Outside passive calibration load
D1, D2	Pyroelectric detectors and Winston cones
F1, F2	Low-pass filters
M1	Tipping mirror
M2	Paraboloidal mirror
P1, P2, P3	Wire grid polarizer
RL	Reference load
RM1, RM2	Roof mirrors
TL1, TL2	Background termination loads

- Based on JASCO-built NRO site testing interferometer design (Matsuo, et al. PASJ **50** 359 1998)
- Commercialized by JASCO as FARIS-1 lab spectrometer
- Modify for access to both polarizations at input and output

# FTS sensitivity

$$SNR = \frac{P}{NEP \cdot t^{-1/2}} \quad P = I \cdot E \cdot \Delta f \cdot \eta$$

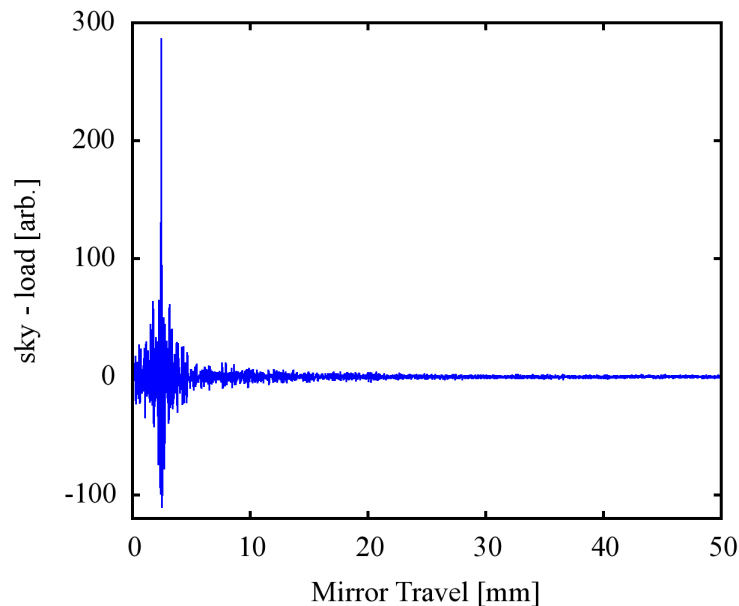
$I$  = radiance

$\Delta f$  = resolution bandwidth

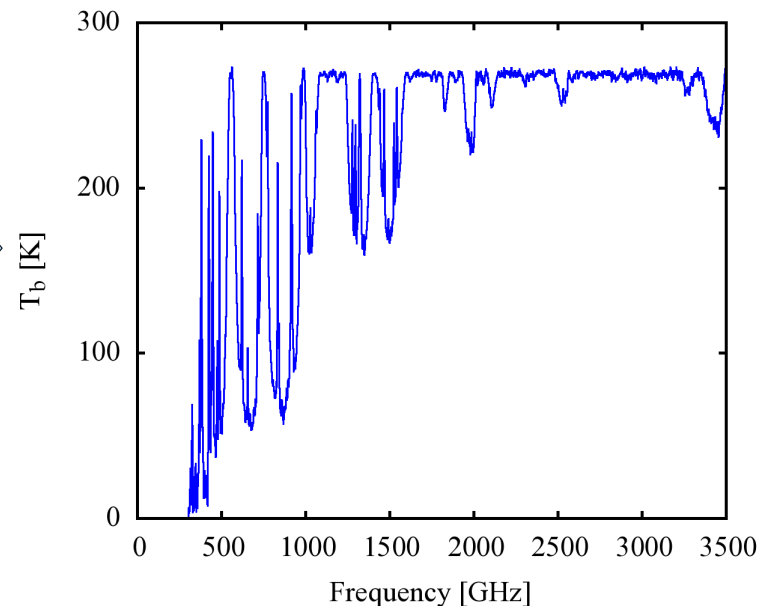
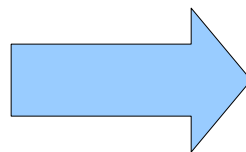
$E$  = optical throughput

$\eta$  = efficiency (assume 0.1)

# FTS dynamic range



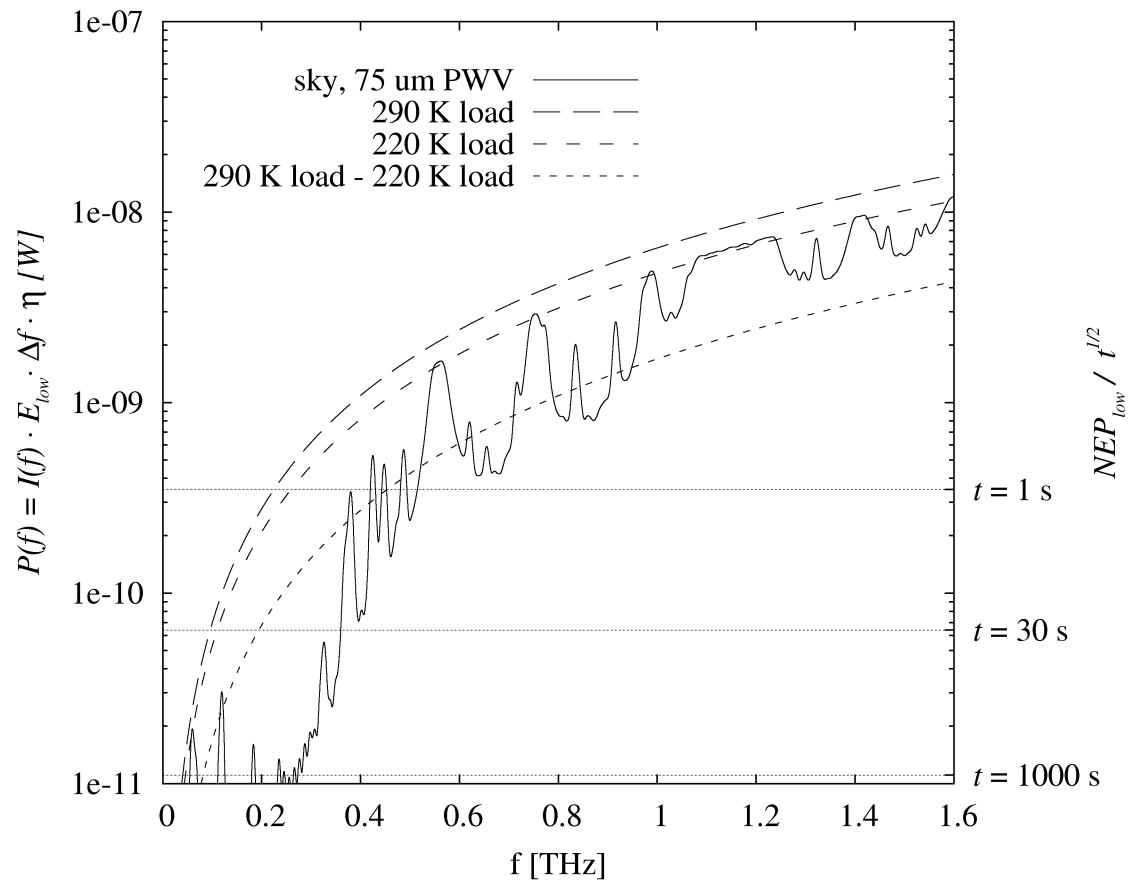
Measured interferogram



Resulting spectrum

Because of the large dynamic range of the interferogram, good linearity and stability are needed to achieve theoretical sensitivity.

# Low band sensitivity



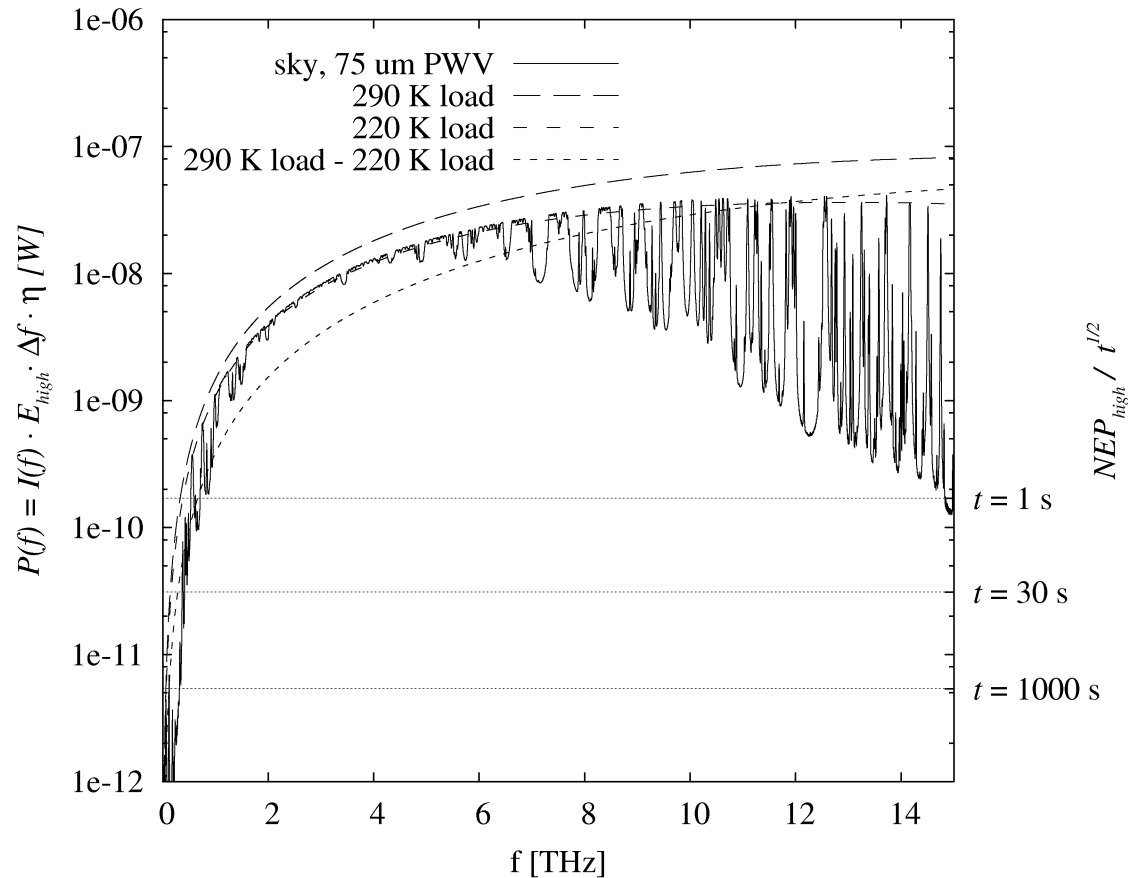
Assumptions:

$$E_{low} = 0.79 \text{ cm}^2 \cdot \text{sr} \text{ (maximum possible for JASCO interferometer)}$$

$$NEP_{low} = 3.5 \cdot 10^{-10} \text{ watt} \cdot \text{Hz}^{-1/2} \text{ (DLATGS detector)}$$

$$\Delta f = 10 \text{ GHz}$$

# High band sensitivity



Assumptions:

$$E_{high} = 0.18 \text{ cm}^2 \cdot \text{sr} \text{ (limited by shortest wavelength)}$$

$$NEP_{high} = 1.7 \cdot 10^{-10} \text{ watt} \cdot \text{Hz}^{-1/2} \text{ (DLATGS detector)}$$

$$\Delta f = 10 \text{ GHz}$$

# Next steps

- Meet with vendor to finalize spectrometer design
  - This week
- Establish integration and deployment timeline
  - This week
- Window, sky mirror, and cal load design and fabrication
  - copy pre-HEAT tipping mirror design?
- Computing and software
  - Migrate vendor system to low-power embedded hardware and OS compatible with existing systems at Dome A